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## Numerical analysis of an isotropic phase-field model with magnetic-field effect



*Analyse numérique d'un modèle isotrope de champ de phase sous l'effet d'un champ magnétique*

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### ABSTRACT

The aim of this letter is to perform the numerical analysis of an isotropic phase-field model for dendritic solidification of a binary alloy subject to an applied magnetic field in an isothermal environment. Precisely, the numerical stability and error analysis of a finite-element-based approximation scheme are performed. The particular example of a nickel–copper (Ni–Cu) binary alloy is considered. The study substantiates a good agreement between the numerical and theoretical results.

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### RÉSUMÉ

Le but de cette note est d'effectuer l'analyse numérique d'un modèle isotrope de champ de phase pour la solidification dendritique d'un alliage binaire sous l'effet d'un champ magnétique appliqué dans un environnement isotherme. Précisément, la stabilité numérique et l'analyse d'erreur du schéma d'approximation éléments finis sont effectuées. L'exemple particulier d'un alliage binaire nickel–cuivre (Ni–Cu) est considéré. L'étude montre un bon accord entre les résultats numériques et théoriques.

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## 1. Introduction

The understanding and control over the evolution of dendrites during the solidification process of metals and alloys has a critical impact on the final solidified material [8]. The phase-field models allowed several investigators to unveil the peculiarities of the synthesis and dynamics of materials during the past couple of decades [1,3,8,15,16], albeit these models are unable to render control over dendrite growth and micro-segregation stand-alone. Nevertheless, experimental studies indicate that the control can be procured in the solidification process by virtue of applied external electric and magnetic fields [4,5,7,13].

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Recently, Rasheed and Belmiloudi [10–12] developed a phase-field model taking care of convection as well as magnetic field. Primarily, the two-dimensional model by Warren and Boettinger [16] for the nickel–copper (Ni–Cu) binary alloy is considered and then the effects of convection in the phase-field and solute equations, and melt–flow equations in the presence of an externally applied magnetic field are included. We refer to [11] for detailed description of the model and [10] for associated mathematical analysis.

The aim of this note is to provide a numerical scheme based on a finite-element method, and a numerical error and stability analysis for the model proposed by Rasheed and Belmiloudi in an isotropic and isothermal regime. In the next section, we briefly provide the mathematical model. Section 3 is dedicated to the variational formulation. Finally, the stability and error analyses are performed in Section 4.

## 2. Mathematical formulation

Let  $\Omega \subset \mathbb{R}^2$  be a sufficiently smooth open solidification domain with regular boundary  $\partial\Omega$  and  $t \in (0, T)$  denote the temporal variable with final solidification time  $T$ . In the sequel, we entertain the following phase-field model for dendrite solidification due to Rasheed and Belmiloudi [10–12]. Let  $\mathbf{u}$ ,  $p$ ,  $\psi$ ,  $c$  and  $\mathbf{B}$  represent the velocity, pressure, phase, concentration and applied magnetic fields, respectively. Then, in the absence of phase and concentration exchange across, and negligible melt velocity along  $\partial\Omega$

$$\begin{cases} \rho_0(\partial_t \mathbf{u} + (\mathbf{u} \cdot \nabla) \mathbf{u}) = -\nabla p + \mu \Delta \mathbf{u} + \mathcal{A}(\psi, c) + b(\psi)((\mathbf{u} \times \mathbf{B}) \times \mathbf{B}), & \Omega \times (0, T), \\ \nabla \cdot \mathbf{u} = 0, & \Omega \times (0, T), \\ \partial_t \psi + (\mathbf{u} \cdot \nabla) \psi = \epsilon_1 (\Delta \psi - \mathcal{H}_1^{\lambda, \delta}(\psi, c)), & \Omega \times (0, T), \\ \partial_t c + (\mathbf{u} \cdot \nabla) c = \nabla \cdot (D(\psi) \nabla c) + \nabla \cdot (\mathcal{H}_2^{\lambda, \delta}(\psi, c) \nabla \psi), & \Omega \times (0, T), \\ (\mathbf{u}, \psi, c) = (\mathbf{u}_0, \psi_0, c_0), & \Omega \times \{0\}, \\ \mathbf{u} = 0, \quad \nabla \psi \cdot \mathbf{n} = 0, \quad \nabla c \cdot \mathbf{n} = 0, & \partial\Omega \times (0, T), \end{cases} \quad (1)$$

where  $\rho_0$  and  $\mu$  are the average density and viscosity,  $D(\psi)$  is the diffusion coefficient,  $\mathbf{n}$  is the unit outward normal and  $\epsilon_1 = M_\psi \epsilon_0^2$  with interface mobility and energy constants  $M_\psi > 0$  and  $\epsilon_0$ . Here  $\mathcal{H}_1^{\lambda, \delta}$ ,  $\mathcal{H}_2^{\lambda, \delta}$  and  $\mathcal{A}$  are defined by

$$\mathcal{H}_1^{\lambda, \delta}(\psi, c) = \frac{\lambda_1(c)}{\delta^2} g'(\psi) + \frac{\lambda_2(c)}{\delta} \bar{p}'(\psi), \quad \mathcal{H}_2^{\lambda, \delta} = \alpha_0 D(\psi) c(1-c) \left( \frac{\lambda_1'(c)}{\delta} g'(\psi) - \lambda_2'(c) \bar{p}'(\psi) \right), \quad (2)$$

$$\mathcal{A} = \beta_c a_1(\psi) c \mathbf{G}, \quad (3)$$

and  $b(\psi) = \sigma_e a_2(\psi)$  where *prime* denotes the ordinary derivative with respect to the variable involved,  $\sigma_e$  is the electric conductivity,  $\mathbf{G}$  is the gravity vector,  $\beta_c$  is the solutal expansion coefficient,  $\delta$  is the interface thickness,  $\alpha_0$  is a material parameter,  $\lambda_i$  ( $i = 1, 2$ ) are linear functions involving material-dependent constants and,  $g$ ,  $\bar{p}$ ,  $a_1$  and  $a_2$  are included for modeling convenience satisfying the conditions  $g(0) = g(1) = 0$ ,  $g'(\psi) = 0 \iff \psi \in \{0, 1, 1/2\}$ ,  $g''(0), g''(1) > 0$ ,  $g(\psi) = g(1 - \psi)$ ,  $\bar{p}(0) = \bar{p}(1) = 0$ ,  $\bar{p}'(\psi) > 0$  for all  $\psi \in (0, 1)$  and  $a_i(0) = 0$  ( $i = 1, 2$ ). Throughout this study, we assume  $a_1(\psi) = \psi$ ,  $\bar{p}(\psi) = \psi^3(10 - 15\psi + 6\psi^2)$  and  $g(\psi) = \bar{p}'(\psi)/30$ . We refer the reader to [11] for a detailed exposition.

## 3. Discrete weak formulation

Let  $(\mathbf{u}, \mathbf{v}) = \int_\Omega \mathbf{u} \cdot \mathbf{v} \, d\mathbf{x}$  and define  $\mathcal{W} = \{\mathbf{v} \in (H^1(\Omega))^2 \mid \mathbf{v}_{\partial\Omega} = 0\}$ ,  $\mathcal{H} = \{q \in L^2(\Omega) \mid \int_\Omega q \, d\mathbf{x} = 0\}$  and  $\mathcal{M} = H^1(\Omega)$ . Let  $h$  be the spatial discretization parameter such that  $0 < h < h_0 < 1$  and  $\mathcal{T}_h$  be a triangulation of  $\Omega$ . Consider the  $\mathbb{P}_l$ ,  $\mathbb{P}_{l-1}$  and  $\mathbb{P}_l$  finite element subspaces  $\mathcal{W}_h$ ,  $\mathcal{H}_h$  and  $\mathcal{M}_h$  of  $\mathcal{W}$ ,  $\mathcal{H}$  and  $\mathcal{M}$  respectively over  $\mathcal{T}_h$ , where  $\mathbb{P}_l$  is the space of polynomials with total degree at most  $l$ . Furthermore, we make the following assumptions.

(A1)  $\exists c_1 > 0$  s.t.  $\forall \mathbf{X} = (\mathbf{u}, \psi, c) \in (H^{r+1}(\Omega))^4 \cap (\mathcal{W} \times \mathcal{M}^2)$  and  $r \in [1, l]$ ,

$$\inf_{\mathbf{X}_h \in \mathcal{W}_h \times \mathcal{M}_h^2} \|\mathbf{X} - \mathbf{X}_h\| \leq c_1 h^r \|\mathbf{X}\|_{H^{r+1}(\Omega)}.$$

(A2)  $\exists c_2 > 0$  s.t.  $\forall q \in H^r(\Omega) \cap \mathcal{H}$  and  $r \in [1, l]$ ,  $\inf_{q_h \in \mathcal{H}_h} \|q - q_h\| \leq c_2 h^r \|q\|_{H^r(\Omega)}$ .

(A3)  $\exists c_3 > 0$  s.t. (*Inf–Sup condition*)  $\inf_{q_h \in \mathcal{H}_h} \sup_{\mathbf{v}_h \in \mathcal{W}_h} \frac{c_p(\mathbf{v}_h, q_h)}{\|\mathbf{v}_h\| \|q_h\|} \geq c_3$ , where  $c_p(\mathbf{u}, p) = -(\nabla \cdot \mathbf{u}, p)$ .

(A4) Let  $\mathbf{X}_0 = (\mathbf{u}_0, \psi_0, c_0) \in (H^{r+1}(\Omega))^4$  for  $r \in [1, l]$ , then  $h \|\mathbf{X}_0 - \mathbf{X}_{0h}\| + |\mathbf{X}_0 - \mathbf{X}_{0h}| \leq c_4 h^{r+1}$ , where  $\mathbf{X}_{0h} = (\mathbf{u}_{0h}, \psi_{0h}, c_{0h}) \in \mathcal{W}_h \times \mathcal{M}_h^2$  is the approximation of  $\mathbf{X}_0$ .

(A5) For all integers  $m, p, q$  and  $\ell$  with  $0 < p, q \leq \infty$  and for all simplex  $K \in \mathcal{T}_h$ , we have:

$$\|\mathbf{X}_h\|_{W^{m, q}(K)} \leq c_4 h^{n/q - n/p + \ell - m} \|\mathbf{X}_h\|_{W^{\ell, p}(K)}, \quad \forall \mathbf{X}_h \in \mathcal{W}_h \times \mathcal{M}_h^2.$$

Consider the following discrete weak form of (1), wherein we use artificial source terms  $F_u$ ,  $F_\psi$  and  $F_c$  for fabricating exact solutions thereby analyzing the convergence and stability of the numerical scheme.

Discrete weak form Find  $(\mathbf{u}_h, p_h, \psi_h, c_h) \in \mathcal{W}_h \times \mathcal{H}_h \times \mathcal{M}_h \times \mathcal{M}_h$  such that  $\forall (\mathbf{v}_h, q_h, \phi_h, z_h) \in \mathcal{W}_h \times \mathcal{H}_h \times \mathcal{M}_h \times \mathcal{M}_h$

$$\left\{ \begin{array}{l} \rho_0(\partial_t \mathbf{u}_h, \mathbf{v}_h) + a_u(\mathbf{u}_h, \mathbf{v}_h) + b_u(\mathbf{u}_h, \mathbf{u}_h, \mathbf{v}_h) + c_p(\mathbf{v}_h, p_h) - (\mathcal{A}(\psi_h, c_h), \mathbf{v}_h) \\ - (b(\psi_h)((\mathbf{u}_h \times \mathbf{B}) \times \mathbf{B}), \mathbf{v}_h) = (\mathbf{F}_u, \mathbf{v}_h), \\ c_p(\mathbf{u}_h, q_h) = 0, \\ (\partial_t \psi_h, \phi_h) + a_\psi(\psi_h, \phi_h) + b_\psi(\mathbf{u}_h, \psi_h, \phi_h) + \epsilon_1(\mathcal{H}_1^{\lambda, \delta}(\psi_h, c_h), \phi_h) = (F_\psi, \phi_h), \\ (\partial_t c_h, z_h) + b_c(\mathbf{u}_h, c_h, z_h) + (D(\psi_h)\nabla c_h, \nabla z_h) + (\mathcal{H}_2^{\lambda, \delta}(\psi_h, c_h)\nabla \psi_h, \nabla z_h) = (F_c, z_h), \\ (\mathbf{u}_h, \psi_h, c_h)(t=0) = (\mathbf{u}_{0h}, \psi_{0h}, c_{0h}), \\ a_u(\mathbf{u}, \mathbf{v}) = \mu \int_{\Omega} \nabla \mathbf{u} \cdot \nabla \mathbf{v} \, d\mathbf{x}, \quad a_\psi(\psi, \phi) = \epsilon_1 \int_{\Omega} \nabla \psi \cdot \nabla \phi \, d\mathbf{x}, \quad b_c(\mathbf{u}, c, z) = \sum_{i=1}^2 \int_{\Omega} u_i(\partial_i c)z \, d\mathbf{x}, \\ b_u(\mathbf{u}, \mathbf{v}, \mathbf{w}) = \rho_0 \sum_{i,j=1}^2 \int_{\Omega} u_i(\partial_i v_j)w_j \, d\mathbf{x}, \quad b_\psi(\mathbf{u}, \psi, \phi) = \sum_{i=1}^2 \int_{\Omega} u_i(\partial_i \psi)\phi \, d\mathbf{x}. \end{array} \right. \quad (4)$$

Let  $(\varphi_{ih})_1^M$ ,  $(q_{ih})_{2M+1}^{2M+N}$  and  $(z_{ih})_{2M+N}^{2M+N+\tilde{M}}$  be the basis of  $\mathcal{W}_h$ ,  $\mathcal{H}_h$  and  $\mathcal{M}_h$  respectively and

$$\mathbf{u}_h = \sum_{i=1}^M \mathbf{u}_{ih} \varphi_{ih} = \sum_{i=1}^M u_{ih} \underline{\varphi}_{ih}^u + \sum_{i=1}^M v_{ih} \underline{\varphi}_{ih}^v, \quad p_h = \sum_{i=2M+1}^{2M+N} p_{ih} q_{ih}, \quad (5)$$

$$\psi_h = \sum_{i=2M+N+1}^{2M+N+\tilde{M}} \psi_{ih} z_{ih}, \quad c_h = \sum_{i=2M+N+\tilde{M}+1}^{2M+N+2\tilde{M}} c_{ih} z_{ih}, \quad (6)$$

where  $\mathbf{u}_{ih} = (u_{ih} \ v_{ih})^t$ ,  $\underline{\varphi}_{ih}^u = (\varphi_{ih} \ 0)^t$ ,  $\underline{\varphi}_{ih}^v = (0 \ \varphi_{ih})^t$ .

By virtue of (5), the semi-discrete weak form (4) yields the differential-algebraic system

$$\mathbb{M} \frac{d\mathbf{Y}_h}{dt} + \mathbb{A}(\mathbf{Y}_h)\mathbf{Y}_h + \mathbf{L}(\mathbf{Y}_h) = \mathbf{R}, \quad \mathbf{Y}_h(t=0) = \mathbf{Y}_{0h}, \quad (7)$$

$$\mathbf{Y}_h = (\mathbf{u}_{1h} \cdots \mathbf{u}_{Mh} \ p_{1h} \cdots p_{Nh} \ \psi_{1h} \cdots \psi_{\tilde{M}h} \ c_{1h} \cdots c_{\tilde{M}h})^t, \quad (8)$$

where  $\mathbf{R} = (R_1 \ 0 \ R_3 \ R_4)^t$ ,  $\mathbf{L}(\mathbf{Y}_h) = (L_1 \ 0 \ L_3 \ 0)^t$  and, for  $K_1 = 2M + N + 2\tilde{M}$  and  $K_2 = 2M + N + 2\tilde{M}$

$$\mathbb{M} = \begin{pmatrix} M_{11} & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & M_{33} & 0 \\ 0 & 0 & 0 & M_{44} \end{pmatrix} \in \mathbb{R}^{K_1 \times K_2}, \quad \mathbb{A}(\mathbf{Y}_h) = \begin{pmatrix} A_{11} & A_{12} & 0 & 0 \\ A_{21} & 0 & 0 & 0 \\ 0 & 0 & A_{33} & 0 \\ 0 & 0 & A_{43} & A_{44} \end{pmatrix} \in \mathbb{R}^{K_1 \times K_2},$$

with

$$\begin{aligned} (M_{11})_{ji} &= \rho_0(\underline{\varphi}_{ih}^u, \underline{\varphi}_{jh}^u) + \rho_0(\underline{\varphi}_{ih}^v, \underline{\varphi}_{jh}^v), & (M_{33})_{ji} &= (z_{ih}, z_{jh}), & (M_{44})_{ji} &= (z_{ih}, z_{jh}), \\ (A_{11})_{ji} &= a_u(\underline{\varphi}_{ih}^u, \underline{\varphi}_{jh}^u) + a_u(\underline{\varphi}_{ih}^v, \underline{\varphi}_{jh}^v) + b_u(\mathbf{u}_h; \underline{\varphi}_{ih}^u, \underline{\varphi}_{jh}^u) + b_u(\mathbf{u}_h, \underline{\varphi}_{ih}^v, \underline{\varphi}_{jh}^v) \\ &\quad - (b(\psi_h)((\underline{\varphi}_{ih}^u \times \mathbf{B}) \times \mathbf{B}), \underline{\varphi}_{jh}^u) - (b(\psi_h)((\underline{\varphi}_{ih}^v \times \mathbf{B}) \times \mathbf{B}), \underline{\varphi}_{jh}^v), \\ (A_{12})_{ji} &= (q_{ih}, \nabla \cdot (\underline{\varphi}_{jh}^u)) + (q_{ih}, \nabla \cdot (\underline{\varphi}_{jh}^v)) = (A_{21})_{ij}, & (A_{33})_{ji} &= a_\psi(z_{ih}, z_{jh}) + b_\psi(\mathbf{u}_h, z_{ih}, z_{jh}), \\ (A_{43})_{ji} &= (\mathcal{H}_2^{\lambda, \delta}(\psi_h, c_h)\nabla z_{ih}, \nabla z_{jh}), & (A_{44})_{ji} &= (D(\psi_h)\nabla z_{ih}, \nabla z_{jh}) + b_c(\mathbf{u}_h, z_{ih}, z_{jh}), \\ (L_1)_j &= (\mathcal{A}_1(\psi_h, c_h), \underline{\varphi}_{jh}^u) + (\mathcal{A}_1(\psi_h, c_h), \underline{\varphi}_{jh}^v), & (L_3)_j &= \epsilon_1(\mathcal{H}_1^{\lambda, \delta}(\psi_h, c_h), z_{jh}), \\ (R_1)_j &= (\mathbf{F}_u, \underline{\varphi}_{jh}^u) + (\mathbf{F}_u, \underline{\varphi}_{jh}^v), & (R_3)_j &= (F_\psi, z_{jh}), & (R_4)_j &= (F_c, z_{jh}). \end{aligned}$$

Let  $\mathbf{u}_i = \mathbf{u}(t_i)$ ,  $t_i = i\tau$  ( $0 \leq i \leq k$ ) where  $\tau$  is the temporal step size,  $\Psi_h = (\mathbf{u}_h, \psi_h, c_h)$ ,  $\Psi = (\mathbf{u}, \psi, c)$  and  $\mathbb{Y}$  be a Banach space. We define

$$\ell^p(0, T, \mathbb{Y}) = \left\{ \mathbf{u} : (t_1, \dots, t_k) \rightarrow \mathbb{Y} \mid \|\mathbf{u}\|_{\ell^p(0, T, \mathbb{Y})}^p = \left( \tau \sum_{i=1}^k \|\mathbf{u}_i\|_{\mathbb{Y}}^p \right) < \infty \right\}.$$

Then, the following error estimates can be obtained; see, for instance, [2,9,14]

$$\|\Psi_h - \Psi\|_{\ell^2(0, T, L^2(\Omega))} \leq C(\tau^\alpha + h^{\beta_1}) \quad \text{and} \quad \|p_h - p\|_{\ell^2(0, T, L^2(\Omega))} \leq C(\tau^\alpha + h^{\beta_2}), \quad (9)$$

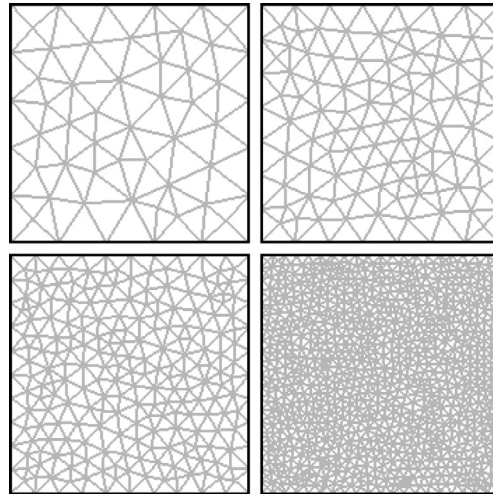


Fig. 1. Meshes.

**Table 1**  
Mesh statistics.

Mesh	$h$	Elements	Boundary elements
1	0.2	106	5
2	0.15	200	7
3	0.1	434	10
4	0.05	1712	20

for some  $\beta_1, \beta_2 > 1$  and  $\alpha \geq 1$ . Note that  $\beta_i$  ( $i = 1, 2$ ) are less than the minimum degree of the finite elements (polynomials) and the Sobolev space regularity of the solutions. Moreover, for optimal spatial (resp. temporal) convergence rate  $\tau \leq h^{\beta_i}$  (resp.  $h^{\beta_i} < \tau$ ).

#### 4. Analysis of the numerical scheme

In this section, we analyze numerical error and stability to validate the numerical scheme. The system (7) is fully discretized first by invoking Euler's backward difference method and then resolved by using the Newton iteration technique on the resulting non-linear fixed-point system, whereas we have made use of the solver DASSL [6]. The values of the physical parameters are consistent with that in [16] and the constants for the melt-flow equations are chosen in accordance with the physical properties of the nickel-copper (Ni-Cu) system; see, for example [9,11].

In the sequel, we choose  $T = 1$ ,  $\Omega = [0, 2\pi] \times [0, 2\pi]$ ,  $\mathbf{B} = \frac{1}{\sqrt{2}}(1, 1)$  and entertain the following fabricated exact solution to (1) obtained by exploiting the artificial source terms  $\mathbf{F}_u$ ,  $F_\psi$  and  $F_c$ ,

$$\mathbf{u}_{\text{ex}} = \left( \frac{2e^{1-t}}{4\pi^2} \sin(x)^2 y \left(1 - \frac{y}{2\pi}\right) \left(1 - \frac{y}{\pi}\right) - \frac{2e^{1-t}}{4\pi^2} \sin(x) \cos(x) y^2 \left(1 - \frac{y}{2\pi}\right)^2 \right)^t,$$

$$p_{\text{ex}} = e^{1-t} \cos(y), \quad \psi_{\text{ex}} = \frac{e^{1-t}}{2} (\cos(x) \cos(y) + 1), \quad c_{\text{ex}} = \frac{2e^{1-t}}{\pi^2} x^2 \left(1 - \frac{x}{2\pi}\right)^2 (\cos(y) + 1).$$

Furthermore, we consider a sequence of four meshes with a decreasing step  $h$  (see Fig. 1 and Table 1) and use Lagrange  $\mathbb{P}_2$  elements for velocity, phase-field and concentration, and  $\mathbb{P}_1$  elements for pressure.

##### 4.1. Numerical error analysis

In Fig. 2,  $L^2$ -norms of errors in  $\mathbf{u}$ ,  $p$ ,  $\psi$  and  $c$  are plotted versus  $h$  (left) and  $\tau$  (right) in  $\log$ -scales. For  $h$ -curves, we used  $\tau = 0.01$  and  $0.001$  for linear and quadratic elements, respectively. It is observed that the slopes of the error curves for velocity, phase-field and concentration are approximately 3, whereas that for the pressure is 2; refer to Table 2. For  $\tau$ -curves slopes of all the curves are approximately 1, i.e.  $\alpha = 1$ . Both of these numerical estimates are in good agreement with the postulated error estimate (9).

##### 4.2. Numerical stability analysis

In order to ascertain the numerical stability of the model, we include  $(1 - \epsilon \text{randf})$  in the artificial source terms to introduce  $\epsilon$ -perturbations in the numerical solution, where random function  $\text{randf}$  assumes values in  $[0, 1]$  and  $\epsilon$  is the perturbation control parameter. We fix  $h = 0.2$  and  $\tau = 0.1$ .

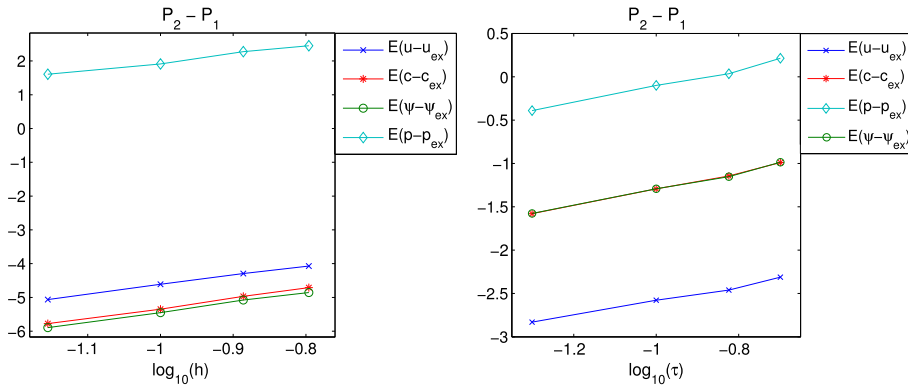


Fig. 2. (Color online.) Error curves with respect to spatial (left) and temporal (right) step size.

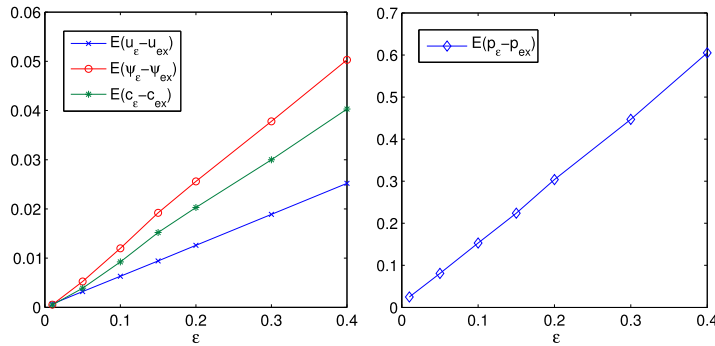


Fig. 3. (Color online.)  $E(\Phi_\epsilon - \Phi_{ex})$  versus  $\epsilon$ .

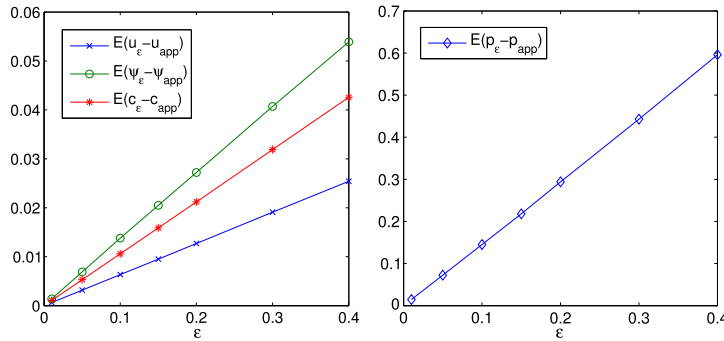


Fig. 4. (Color online.)  $E(\Phi_\epsilon - \Phi_{app})$  versus  $\epsilon$ .

Table 2  
Estimated  $\beta_i$ ,  $i = 1, 2$ .

$\beta_1$ for $\mathbf{u}$ with $\mathbb{P}_2$	2.7501
$\beta_2$ for $p$ with $\mathbb{P}_1$	1.8426
$\beta_1$ for $\psi$ with $\mathbb{P}_2$	2.8001
$\beta_1$ for $c$ with $\mathbb{P}_2$	2.8449

Table 3  
Slopes of norm  $L_2$ .

Slope	$E(\Phi_\epsilon - \Phi_{ex})$
$m_{\mathbf{u}}$	0.0628
$m_\psi$	0.1276
$m_c$	0.1021
$m_p$	1.4738

We perform three different stability tests in Figs. 3–5. In Fig. 3, the  $L^2$ -norm of the discrepancy between exact solution  $\Phi_{ex} = (\mathbf{u}_{ex}, p_{ex}, \psi_{ex}, c_{ex})$  and its  $\epsilon$ -perturbation  $\Phi_\epsilon = (\mathbf{u}_\epsilon, p_\epsilon, \psi_\epsilon, c_\epsilon)$ , i.e.  $E(\Phi_\epsilon - \Phi_{ex}) = \|\Phi_\epsilon - \Phi_{ex}\|_{L_2}$  is plotted versus  $\epsilon$ . A linear dependence of error on  $\epsilon$  is observed, indeed,  $E(\Phi_\epsilon - \Phi_{ex}) \approx m_s \epsilon$  where  $m_s$  ( $s = u, p, \psi, c$ ) represents the slope of the error curve; refer to Table 3. In Fig. 4,  $E(\Phi_\epsilon - \Phi_{app}) = \|\Phi_\epsilon - \Phi_{app}\|_{L_2}$  is plotted against  $\epsilon$  where  $\Phi_{app} = (\mathbf{u}_{app}, p_{app}, \psi_{app}, c_{app})$  is the approximate solution without random error (i.e.  $\epsilon = 0$ ). The same observation holds as in Fig. 4; refer also to Table 4. Finally, in Fig. 5, the solution curves for different perturbation levels  $\epsilon$  are delineated on a part of the domain in order to establish stability with respect to random perturbations. We fix  $t = 1$ ,  $y = \pi$  and  $x \in [0, 1]$  for velocity and,  $t = 1$ ,  $x = \pi$  and  $y \in [0, 1]$  for pressure, phase field and concentration. The graphs substantiate that the solution is indeed stable.

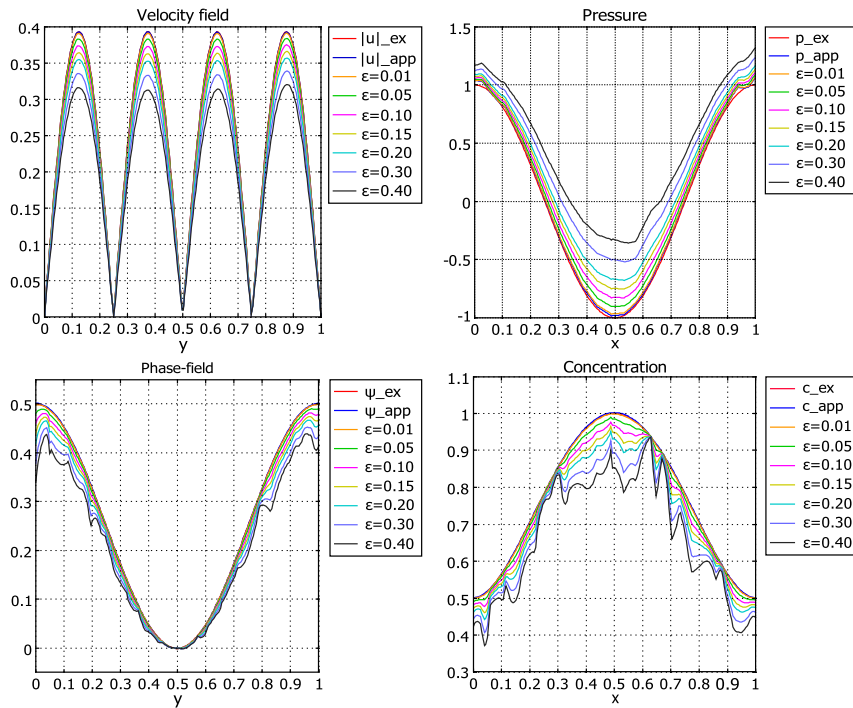


Fig. 5. (Color online.) Solution curves for the different values of  $\epsilon$ .

Table 4

Slopes of norm  $L_2$ .

Slope	$E(\Phi_\epsilon - \Phi_{app})$
$m_u$	0.0628
$m_\psi$	0.1277
$m_c$	0.1028
$m_p$	1.4913

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